

STORMWATER MANAGEMENT PLAN
JOSHUA COURT SUBDIVISION
WEST LINCOLN

Prepared for:

RVL Homes

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REFERENCES

1. Stormwater Management Planning and Design Manual
Ontario Ministry of Environment (March 2003)

STORMWATER MANAGEMENT PLAN

JOSHUA COURT SUBDIVISION

TOWN OF WEST LINCOLN

1.0 INTRODUCTION

1.1 Study Area

The proposed subdivision is located in the Township of West Lincoln as part of the hamlet settlement area of Allen Corners. The subject property is situated south of Young Street, north of Regional Road 20 and east of Grimsby Road (Regional Road 12). This Stormwater Management Plan has been prepared as part of the Draft Plan of Subdivision Process.

The area of the development is approximately 4.27 ha with 3.17 ha within the hamlet and is bound by agricultural lands to the east and existing single residential properties along the north and south boundaries. The drainage areas contributing to this stormwater management plan consist primarily of the subject lands and external northerly land. The receiving body of water for the proposed stormwater flows will be a Tributary of Twenty Mile Creek.

1.2 Objectives

The objectives of this study are as follows:

1. Establish specific criteria for the management of stormwater from this site.
2. Determine the impact of development on the stormwater peak flow & volume from this site.
3. Establish property requirements for the Stormwater Management Facility for the Draft Plan of Subdivision

1.3 Existing & Proposed Conditions

a) Existing Conditions

The subject land use is agricultural. The lands generally convey stormwater flows to either the Grimsby Road (Regional Road 12) roadside ditch or to a tributary of Twenty Mile Creek located at the southeast limits of the site. All flows are part of Twenty Mile Creek located south of the site.

b) Proposed Conditions

As part of the development, 6 residential lots will be created for rural single residential uses. A 0.13 hectare block (Block 7) is provided for Stormwater Management practices. As no sanitary sewer or watermain exists in proximity to the site, each dwelling will be constructed with an associated individual private septic system and water system. Roadside ditches will provide drainage for the roadway conveying flows easterly to Block 7.

2.0 STORMWATER MANAGEMENT CRITERIA

New developments are required to provide stormwater management in accordance with provincial and municipal policies including:

- Stormwater Quality Guidelines for New Development (MECP/MNRF, May 1991)
- Stormwater Management Planning and Design Manual (MECP, March 2003)

Based on the above policies and site specific considerations, the following stormwater management criteria have been established for this site.

- The drainage areas of the development direct stormwater to a tributary of Twenty Mile Creek with an MNR Type 2 habitat watercourse. Therefore, Stormwater **quality** controls require MECP Normal Protection to the stormwater before discharging to the Twenty Mile Creek Tributary.
- Stormwater **quantity** controls are to be provided for the outlet to limit the proposed development peak flows from the 5 and 100 year storm events to existing peak flow levels

3.0 STORMWATER ANALYSIS

A stormwater analysis of the Joshua Court Subdivision development has been prepared using the MIDUSS computer modelling program. A stormwater analysis was conducted to represent the existing and proposed conditions to the various site stormwater outlets.

This program was selected because it is applicable to an urban drainage area like the study area, it is relatively easy to use and modify for the proposed drainage conditions and control facilities, and it readily allows for the use of design storm hydrographs for the various return periods being investigated. Copies of the current model output files are enclosed in Appendix B.

3.1 Design Storms

Design storm hydrographs were developed using a Chicago distribution based on the Intensity-Duration-Frequency curves for the development area in West Lincoln. Hydrographs for the 25mm, 5, and 100 year events were developed using a 4 hour Chicago distribution. Table 1 summarizes the rainfall data.

| Table 1. Rainfall Data | | | |
|---|--|----------|----------|
| Design Storm (Return Period) | Chicago Distribution Parameters | | |
| | a | b | c |
| 25mm | 512.000 | 6.000 | 0.800 |
| 5 Year | 3175.000 | 20.000 | 1.000 |
| 100 Year | 6300.000 | 15.000 | 1.000 |
| $Intensity \ (mm/hr) = \frac{a}{(t_d + b)^c}$ | | | |

3.2 Existing Conditions

The existing conditions were modelled to establish the stormwater peak flows and volumes prior to development within this site. The existing drainage areas for the subject lands are shown in Figure 1 outlining the various drainage areas to 4 separate stormwater outlets. These areas were determined from field investigations and a combination of topographic surveys and topographic information from the Regional Niagara DTM.

Outlet A contains the stormwater directed to the Grimsby Road (Regional Road 12) roadside ditch, and is represented by Drainage Area EX2. Outlet B comprises of the stormwater that outlets at the southeast portion of the site through an existing ditch and includes drainage area EX4. Outlet C comprises of the stormwater that outlets at the northeast corner of the site and the tributary of Twenty Mile Creek that crosses through the northeast corner of the site. This outlet includes Drainage Areas EX1 and EX3. Outlet D contains the tributary of Twenty Mile Creek prior to entering the site. Drainage Area EX1 represents the entire drainage area for the tributary for Twenty Mile Creek from the start of the watercourse to Outlet D where it enters the subject lands. Outlet E represents the combination of stormwater from Outlets B and C, that converge southeast of the site.

All stormwater flows from the development site are ultimately conveyed southerly and converge with the tributary of Twenty Mile Creek. Table 3 details the stormwater peak flows generated by the various design storm events.

3.3 Proposed Conditions

The future drainage areas for the proposed development, shown in Figure 2, were modelled to establish the stormwater peak flows once development has been completed at the proposed site. The proposed development will continue to discharge stormwater flows at allowable levels.

Stormwater flows as part of Drainage Area A10 will be directed to the roadside ditch on Grimsby Road (Regional Road 12) outletting at Outlet A. Outlet B will contain Drainage Areas A20, A30, A40 and A70. Drainage areas A30 and A40 will be conveyed through the proposed roadside ditches, Drainage Area A20 will be directed through a series of rear yard swales and Drainage Area A70 will drain directly to Outlet B. Outlet C will contain Drainage Areas A50, A60 and A80. Drainage Areas A50 and A60 will be directed through a series of rear yard swales that will outlet at Outlet C. Drainage Area A80 contains the entire drainage area for the tributary of Twenty Mile Creek before entering the site at Outlet D.

It is proposed to redirect 100m of the tributary of Twenty Mile Creek that crosses the northeast corner of the site between Outlet D to Outlet C. The channel will be redirected to flow easterly directly behind Blocks 5 and 6, and will converge with the proposed-on site ditch in Block 5 at the northeast corner of the site.

Input parameters for the computer model with the proposed development conditions are shown in Table 2. The impervious values for each drainage area have been estimated based on the existing and future land uses with calculations included in Appendix A.

| Table 2. Hydrologic Parameters | | | | | |
|--------------------------------|-----------|------------|-----------|--------|--------------------|
| Area No. | Area (ha) | Length (m) | Slope (%) | SCS CN | Percent Impervious |
| Existing Conditions | | | | | |
| EX1 | 19.77 | 363 | 0.5 | 74 | 7.9 |
| EX2 | 0.42 | 53 | 0.5 | 74 | 42.6 |
| EX3 | 2.23 | 122 | 0.5 | 74 | 5.6 |
| EX4 | 2.29 | 123 | 0.5 | 74 | 3.8 |
| 24.71 | | Total Area | | | |
| Future Conditions | | | | | |
| A10 | 0.45 | 55 | 0.5 | 74 | 40.7 |
| A20 | 1.59 | 103 | 1.0 | 74 | 7.5 |
| A30 | 0.39 | 51 | 0.5 | 74 | 35.1 |
| A40 | 0.37 | 47 | 0.5 | 74 | 39.5 |
| A50 | 1.39 | 92 | 1.0 | 74 | 10.6 |
| A60 | 0.36 | 49 | 1.0 | 74 | 5.4 |
| A70 | 0.39 | 51 | 0.5 | 74 | 6.2 |
| A80 | 19.77 | 363 | 0.5 | 74 | 7.9 |
| 24.71 | | Total Area | | | |

The results of the modelling are shown in Table 3, where the peak flows were calculated for the 5 and 100 year design storm events.

| Table 3. Peak Flows | | | |
|--|------------------------------------|----------------|---------------|
| Design Storm | Peak Flow (m³/s) | | |
| | Existing | Future* | Change |
| <i>Outlet A</i> | | | |
| 5 Year | 0.040 | 0.041 | +2.50% |
| 100 Year | 0.109 | 0.112 | +2.75% |
| <i>Outlet B</i> | | | |
| 5 Year | 0.040 | 0.098 | +145.00% |
| 100 Year | 0.245 | 0.395 | +61.22% |
| <i>Outlet C</i> | | | |
| 5 Year | 0.376 | 0.385 | +2.39% |
| 100 Year | 1.449 | 1.357 | -6.35% |
| <i>Outlet D</i> | | | |
| 5 Year | 0.340 | 0.340 | 0% |
| 100 Year | 1.270 | 1.270 | 0% |
| <i>Outlet E</i> | | | |
| 5 Year | 0.403 | 0.481 | +19.35% |
| 100 Year | 1.649 | 1.717 | +4.12% |
| Note: * Represents future stormwater conditions without stormwater quantity controls | | | |

For the purpose of Table 3, the total peak stormwater flow values discharging to Outlet E is the confluence of peak flows from Outlet B and C that converge east of the subject lands. The future peak flows from the site have been calculated and outlined in this table to provide conclusions regarding the necessity of quantity controls.

As seen in Table 3, the change in stormwater flows at Outlet A and C are negligible during all modelled storm events. However, peak stormwater flows at Outlet B are greatly increased under proposed conditions and stormwater quantity controls will be required. By controlling stormwater flows at Outlet B, the stormwater flows at Outlet E will be reduced.

It is proposed to construct a Dry Pond Stormwater Management Facility within Block 7 to provide the necessary quantity controls to restrict peak stormwater flows to allowable levels prior to discharge from the site. The quantity controls will ensure that the combined future peak stormwater flows discharging to Outlet B from Drainage Areas A20, A30, A40, and A70 will be reduced to allowable levels outlined by Drainage Area EX4.

A0

0.00

0.00

DRAINAGE AREA NUMBER

DRAINAGE AREA IN HECTARES

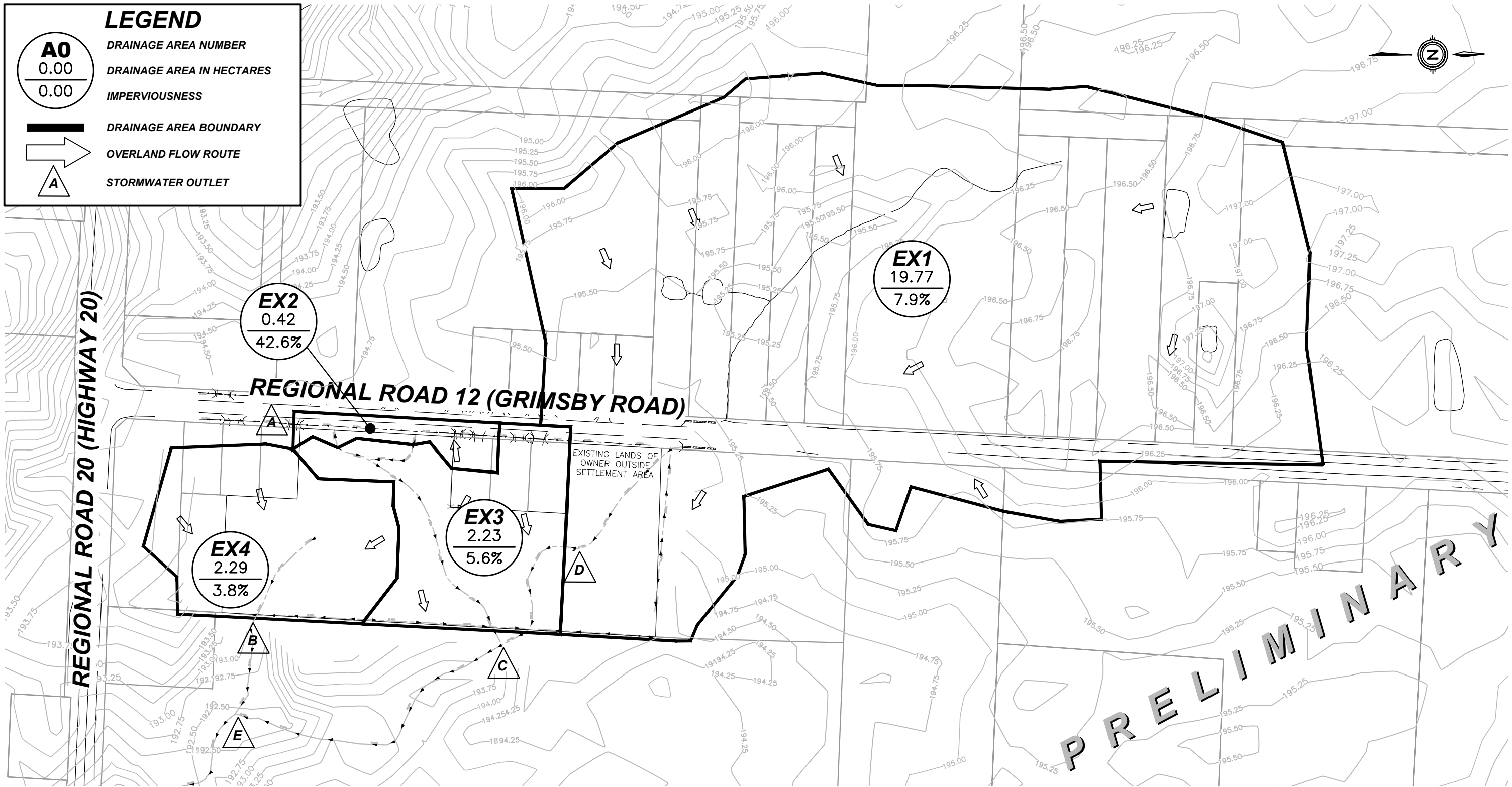
IMPERVIOUSNESS

DRAINAGE AREA BOUNDARY

OVERLAND FLOW ROUTE

A

STORMWATER OUTLET



UPPER CANADA
CONSULTANTS
ENGINEERS / PLANNERS

JOSHUA COURT SUBDIVISION, WEST LINCOLN
EXISTING EXTERNAL STORM DRAINAGE AREA PLAN

DATE 2024-03-12

SCALE 1:2500 m

REF No. 19126

DWG No. FIGURE 1

A0

0.00

0.00

DRAINAGE AREA NUMBER

DRAINAGE AREA IN HECTARES

IMPERVIOUSNESS

DRAINAGE AREA BOUNDARY

OVERLAND FLOW ROUTE

A

STORMWATER OUTLET

LEGEND

- A0**
0.00
0.00
DRAINAGE AREA NUMBER
DRAINAGE AREA IN HECTARES
IMPERVIOUSNESS
- DRAINAGE AREA BOUNDARY**
- OVERLAND FLOW ROUTE**
- STORMWATER OUTLET**

REGIONAL ROAD 20 (HIGHWAY 20)

REGIONAL ROAD 12 (GRIMSBY ROAD)

JOSHUA COURT

EXISTING LANDS OF OWNER OUTSIDE SETTLEMENT AREA

PROPOSED CHANNEL

PROPOSED SWM FACILITY

PRELIMINARY

| Drainage Area | Area (ha) | Imperviousness (%) |
|---------------|-----------|--------------------|
| A0 | 0.00 | 0.00 |
| A10 | 0.45 | 40.7% |
| A20 | 1.59 | 7.5% |
| A30 | 0.39 | 35.1% |
| A40 | 0.37 | 39.5% |
| A50 | 1.39 | 10.6% |
| A60 | 0.36 | 5.4% |
| A70 | 0.39 | 6.2% |
| A80 | 19.77 | 7.9% |

JOSHUA COURT SUBDIVISION, WEST LINCOLN
PROPOSED EXTERNAL STORM DRAINAGE AREA PLAN

| | |
|---------|------------|
| DATE | 2024-03-07 |
| SCALE | 1:2500 m |
| REF No. | 19126 |
| DWG No. | FIGURE 2 |

DRAWING FILE: F:\19126\Engineering\19126-SWM BASE.dwg PLOTTED: Mar 13, 2024 - 8:33am PLOTTED BY: zachb

4.0 STORMWATER MANAGEMENT PLAN

A MIDUSS model was created to assess existing, future and ultimate development peak flows by the proposed subdivision. The stormwater management facility was sized according to MECP Guidelines (MECP, March 2003) as follows:

4.1 Stormwater Quantity Control

As stated previously through conclusions provided from Table 3, stormwater flows discharging to Outlets A and C have a minimal increase compared to existing conditions and quantity controls will not be required. Drainage Area A70 will provide quantity controls to ensure that the combined future peak stormwater flows discharging to Outlet B from Drainage Areas A20, A30, and A40 will be reduced to allowable levels outlined by Drainage Area EX4. Stormwater flows at Outlet E that contain the flows from Outlet B and C will be analysed to ensure the flows are reduced to allowable levels outlined by Drainage Areas EX1, EX3 and EX4.

A Dry Pond located at the east portion of the site in Block 7 will provide the necessary controls to reduce peak flows to allowable levels.

4.1.1 Stormwater Management Facility Configuration

The layout of the stormwater management facility is providing a single outlet at Outlet B, prior to converging with the tributary of Twenty Mile Creek. A dry pond will be located 80 meters north of the outlet and a 600mm diameter pipe slopped at 0.1% will provide an outlet for the dry pond and convey flows to Outlet B. The swale at the southeast corner of the property will provide additional storage. A retaining wall will be constructed beginning at the south side of Outlet B and follow the property line along the rear yard swale in Lot 4 at an elevation of 194.00m to ensure water does not spill over onto the adjacent properties during stormwater controlled events.

To provide the required quantity controls, it is proposed to construct a two-stage headwall at Outlet B. The headwall will have a 0.050m wide slot weir from the base elevation of 192.52m. At an elevation of 193.25m to an elevation of 194.00m at the top of the headwall, the slot weir will increase to 0.2m wide. This will act as an emergency overflow weir to allow stormwater flow to discharge at greatly increased rates during extreme storm events. Storage will be provided by the proposed dry pond, a 600mm diameter pipe that connects the dry pond to the headwall and the southern area of Block 7 swale in Drainage Area A20. See Appendix A for the storage calculations provided by the dry pond and rear yard swale in Drainage Area A20.

Table 4 below outlines the stormwater characteristics experienced by the Stormwater Management Dry Pond Facility during the modelled storm events. Based on the configuration of the facility, a storage volume of approximately 1043.08m³ will be provided for stormwater management. See Appendix A for the Stage Storage Discharge Calculations.

| Table 4. Stormwater Management Facility Characteristics | | | | |
|--|-------------------------|----------------|------------------------------|---------------------------------------|
| Design Storm | Peak Flows (L/s) | | Maximum Elevation (m) | Maximum Volume (m³) |
| | Inflow | Outflow | | |
| 5 Year | 95 | 39 | 193.07 | 215 |
| 100 Year | 391 | 211 | 193.66 | 654 |

Therefore, stormwater within the facility will reach a maximum elevation of 193.66m during the 100-year design storm event. Stormwater levels during all modelled storm events will remain below the overflow weir elevation of 194.00m. A freeboard of 0.34m will be experienced by the dry pond during the 100 year event.

4.1.2 (Outlet B and E) Flow Comparison

The combined peak stormwater flows discharging to Outlet B from Drainage Areas A20, A30, A40 and A70 are outlined in Table 5 below.

| Table 5. Outlet B - Peak Stormwater Flows | | | |
|---|----------------------------------|---------------------------------|-----------------------|
| Design Storm | Existing Peak Flows (L/s) | *Future Peak Flows (L/s) | Percent Change |
| 5 Year | 40 | 39 | -2.50% |
| 100 Year | 245 | 211 | -13.88% |
| Note: * Represents future stormwater conditions with stormwater quantity controls | | | |

Therefore, peak stormwater flows at Outlet B will be reduced to less than existing levels under the proposed Stormwater Management Plan.

The combined peak stormwater flows discharging to Outlet E contains the flows from Outlets B and C (Drainage Areas A20, A30, A40, A50, A60, A70 and A80), is outlined in Table 6 below.

| Table 6. Outlet E - Peak Stormwater Flows | | | |
|---|----------------------------------|---------------------------------|-----------------------|
| Design Storm | Existing Peak Flows (L/s) | *Future Peak Flows (L/s) | Percent Change |
| 5 Year | 403 | 400 | -0.74% |
| 100 Year | 1649 | 1569 | -4.85% |
| Note: * Represents future stormwater conditions with stormwater quantity controls | | | |

Therefore, peak stormwater flows at Outlet E will be reduced to less than existing levels under the proposed Stormwater Management Plan.

4.2 Stormwater Quality Control

The Township of West Lincoln as well as the Regional Niagara require the development to provide stormwater quality enhancements to Normal Protection levels prior to discharge from the site. The majority of the development site, particularly all of Drainage Areas A10, A20, A50, A60, and A70 will consist of rear yards and roof top areas that is considered clean stormwater. The driveways and main roadway area within the site will be the sole significant source of contaminants with the development. It is proposed to utilize the roadside ditches to provide the necessary quality controls for the proposed subdivision.

All stormwater from the roadway and driveways within Drainage Area A30 and A40 will be directed to the proposed roadside ditches. The ditches will ultimately convey stormwater flows to the Dry Pond facility prior to discharge from the site. Drainage Area A30 outlines the drainage area for the south roadside ditch and Drainage Area A40 relates to the north roadside ditch.

The ditches will be designed in accordance with the MECP SWM Planning and Design Manual (2003) to provide the necessary water quality enhancements. Grassed swales designed for water quality treatment should be designed to convey peak stormwater flows during a 4 hour 25mm storm at a velocity of less than 0.5 m/s.

An analysis of the 25mm storm has been completed to model the expected stormwater characteristics in the roadside ditches.

Table 7 below outlines the stormwater characteristics of the roadside ditches utilized within the MIDUSS modelling as well as conclusions observed.

| Table 7. Roadside Ditch Stormwater Characteristics | | | | | |
|---|------------------|-----------------------|--------------------------|------------------------------------|-----------------------|
| Drainage Areas | | Roadside Ditch | | | |
| No. | Area (ha) | Slope (%) | Depth of Flow (m) | Flow Rate (m³/s) | Velocity (m/s) |
| A30 | 0.39 | 0.5 | 0.1 | 0.012 | 0.27 |
| A40 | 0.37 | 0.5 | 0.1 | 0.013 | 0.27 |

As shown in Table 7, the stormwater peak flows and velocities within the proposed roadside ditches will be less than 0.5m/s. Therefore, the internal roadside ditches (Enhanced Swales) will provide sufficient quality enhancements for stormwater discharging from the site.

4.3 Northerly Swale Relocation

As stated previously, it is proposed to redirect 100m of the tributary of Twenty Mile Creek that crosses the northeast corner of the site between Outlet D to Outlet C. The channel will be redirected to flow easterly directly behind Blocks 5 and 6, and will converge with the proposed-on site ditch in Block 5 at the northeast corner of the site. The redirected portion of the channel has been designed to accommodate the 5 year design storm event in Drainage Area A80. The redirected channel will be 0.5 meters deep, 1.2 meters wide at the bottom, and have 3:1 side slopes.

5.0 STORMWATER MANAGEMENT FACILITY MAINTENANCE

5.1 Dry Pond Facility

The dry detention stormwater management facility for this development may be subject to frequent wetting and deposition of sediments as a result of frequent low intensity storm events. The purpose of the dry detention area is to detain peak flows to existing levels. For the initial operation period of the stormwater management facility, the required frequency of maintenance is not definitively known and many of the maintenance tasks will be performed on an 'as required' basis. For example, during the construction phase of the development, there will be a greater potential for increased maintenance frequency, which depends on the maintenance of the upstream oil/grit separator and the effectiveness of the sediment and erosion control techniques employed.

Inspections of the dry detention areas will indicate whether or not maintenance is required. Inspections should be made after every significant storm during the first two years of operation or until all development is completed to ensure the dry detention area is functioning properly. This may translate into an average of six inspections per year. Once all building activity is finalized, inspections shall be performed annually.

The following points should be addressed during inspections of the facility.

Standing water above at the headwall outlet above the base a day or more after a storm may indicate a blockage in the control structure. The blockage may be caused by trash or sediment and a visual inspection would be required to determine the cause.

The dry detention area has been created by excavating a detention area and the integrity of the embankment should be periodically checked to ensure that the side slopes have not sloughed.

Trash removal is an integral part of maintenance and annual clean up, usually in the spring, is a minimum requirement. After this, trash removal is performed on an as required basis on observation of trash build-up during inspections.

Grass cutting is a maintenance activity that is done solely for aesthetic purposes. It is recommended that grass cutting be limited to the upper embankment areas. It should be noted that municipal by-laws may require regular grass maintenance for weed control.

5.2 Internal Roadside Ditches (Enhanced Swales)

For the proposed internal roadside ditches, very minor maintenance will be required. In order to provide optimal enhancement measures, it is suggested that the swales maintain moderately overgrown conditions. Per the MECP Guidelines, grass should be allowed to grow higher than 75mm to enhance the filtration of suspended solids. Regular trimming (i.e. mowing) of the conveyance swales could potentially conclude in adverse effects and will prevent the swales from operating as intended. Frequent inspections should be conducted during the first year of operation and annually during spring to ensure a build-up of sediment does not occur.

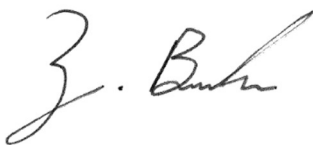
6.0 CONCLUSIONS AND RECOMMENDATIONS

Therefore, based on the above comments and design calculations provided for this site, the following summarizes the stormwater management plan for this site.

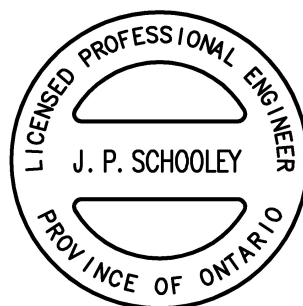
1. Stormwater quality improvements will be provided to Normal Protection by the proposed roadside ditches along Joshua Court, which function as grassed swales in accordance with MECP guidelines.
2. Quantity controls will be provided by the proposed two stage headwall and storage will be provided by the dry pond, a 600mm diameter pipe conveying flows from the dry pond to the headwall and the rear yard swale located in the southeast corner of the site to control the 5 and 100 year storm events to existing conditions.
3. The tributary of Twenty Mile Creek that crosses the northeast corner of the site will be redirected to flow easterly directly behind Blocks 5 and 6, and will converge with the proposed-on site ditch in Block 5 at the northeast corner of the site.

We trust the above comments and enclosed calculations are satisfactory for approval. If you have any questions or require additional information, please do not hesitate to contact our office.

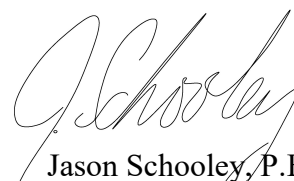
Prepared By:



Zach Barber, E.I.T.



Reviewed By:



Jason Schooley, P.Eng.
Revised March 13, 2024

APPENDICES

APPENDIX A

Weighted Impervious Calculation Sheet
Dry Pond Stage-Storage-Discharge Calculations
Dry-Pond Volume Calculations
A20 Rear Yard Swale Volume Calculations

Weighted Imperviousness Percentage Calculation Worksheet

| | |
|-----------------|--------------------------|
| Project Name: | Joshua Court Subdivision |
| Project Number: | 19126 |
| Date: | February 23, 2024 |
| Person: | Zach Barber |

EX - EXISTING CONDITIONS

| <i>EX1</i> | <i>Footprint</i> | <i>% Impervious</i> | | <i>Effective Impervious Area</i> |
|---|-------------------------|---------------------|----|----------------------------------|
| Existing Buildings, Asphalt Road and Driveways | 15364.5 m ² | 100.0% | ea | 15364.5 m ² |
| Landscape/Greenspace | 182319.6 m ² | 0.1% | ea | 182.3 m ² |
| TOTAL CATCHMENT IMPERVIOUS AREAS | | | | 15,547 m ² |
| TOTAL CATCHMENT AREA | | | | 197,684 m ² |
| EFFECTIVE WEIGHTED CATCHMENT % IMPERVIOUS RUNOFF COEFFICIENT | | | | 7.9 % 0.26 |

EX - EXISTING CONDITIONS

| <i>EX 2</i> | <i>Footprint</i> | <i>% Impervious</i> | | <i>Effective Impervious Area</i> |
|---|-------------------------|---------------------|----|----------------------------------|
| Existing Buildings, Asphalt Road and Driveways | 1787.995 m ² | 100.0% | ea | 1788.0 m ² |
| Landscape/Greenspace | 2411.8 m ² | 0.1% | ea | 2.4 m ² |
| TOTAL CATCHMENT IMPERVIOUS AREAS | | | | 1,790 m ² |
| TOTAL CATCHMENT AREA | | | | 4,200 m ² |
| EFFECTIVE WEIGHTED CATCHMENT % IMPERVIOUS RUNOFF COEFFICIENT | | | | 42.6 % 0.50 |

EX - EXISTING CONDITIONS

| <i>EX3</i> | <i>Footprint</i> | <i>% Impervious</i> | | <i>Effective Impervious Area</i> |
|---|-------------------------|---------------------|----|----------------------------------|
| Existing Buildings, Asphalt Road/Parking Areas & Concrete Apron. | 1237.239 m ² | 100.0% | ea | 1237.2 m ² |
| Landscape/Greenspace | 21049.6 m ² | 0.1% | ea | 21.0 m ² |
| TOTAL CATCHMENT IMPERVIOUS AREAS | | | | 1,258 m ² |
| TOTAL CATCHMENT AREA | | | | 22,287 m ² |
| EFFECTIVE WEIGHTED CATCHMENT % IMPERVIOUS RUNOFF COEFFICIENT | | | | 5.6 % 0.24 |

EX - EXISTING CONDITIONS

| <i>EX4</i> | <i>Footprint</i> | <i>% Impervious</i> | | <i>Effective Impervious Area</i> |
|---|------------------------|---------------------|----|----------------------------------|
| Existing Buildings, Asphalt Road/Parking Areas & Concrete Apron. | 857.3 m ² | 100.0% | ea | 857.3 m ² |
| Landscape/Greenspace | 22023.6 m ² | 0.1% | ea | 22.0 m ² |
| TOTAL CATCHMENT IMPERVIOUS AREAS | | | | 879 m ² |
| TOTAL CATCHMENT AREA | | | | 22,881 m ² |
| EFFECTIVE WEIGHTED CATCHMENT % IMPERVIOUS RUNOFF COEFFICIENT | | | | 3.8 % 0.23 |

Weighted Imperviousness Percentage Calculation Worksheet

Project Name: Joshua Court Subdivision
 Project Number: 19126
 Date: February 23, 2024
 Person: Zach Barber

PROP - PROPOSED CONDITIONS

| A10 | <i>Footprint</i> | <i>% Impervious</i> | | <i>Effective Impervious Area</i> |
|---|-----------------------|---------------------|----|----------------------------------|
| Prop Buildings, Asphalt Road and Driveways | 40.6 m ² | 100.0% | ea | 40.6 m ² |
| Existing Buildings, Asphalt Road and Driveways | 1788.0 m ² | 100.0% | ea | 1788.0 m ² |
| Landscape/Greenspace | 2669.2 m ² | 0.1% | ea | 2.7 m ² |
| TOTAL CATCHMENT IMPERVIOUS AREAS | | | | 1,831 m ² |
| TOTAL CATCHMENT AREA | | | | 4,498 m ² |
| EFFECTIVE WEIGHTED CATCHMENT % IMPERVIOUS RUNOFF COEFFICIENT | | | | 40.7 % 0.49 |

PROP - PROPOSED CONDITIONS

| A20 | <i>Footprint</i> | <i>% Impervious</i> | | <i>Effective Impervious Area</i> |
|---|------------------------|---------------------|----|----------------------------------|
| Prop Buildings, Asphalt Road and Driveways | 312.7 m ² | 100.0% | ea | 312.7 m ² |
| Existing Buildings, Asphalt Road and Driveways | 857.3 m ² | 100.0% | ea | 857.3 m ² |
| Landscape/Greenspace | 14696.2 m ² | 0.1% | ea | 14.7 m ² |
| TOTAL CATCHMENT IMPERVIOUS AREAS | | | | 1,185 m ² |
| TOTAL CATCHMENT AREA | | | | 15,866 m ² |
| EFFECTIVE WEIGHTED CATCHMENT % IMPERVIOUS RUNOFF COEFFICIENT | | | | 7.5 % 0.25 |

PROP - PROPOSED CONDITIONS

| A30 | <i>Footprint</i> | <i>% Impervious</i> | | <i>Effective Impervious Area</i> |
|---|-----------------------|---------------------|----|----------------------------------|
| Prop Buildings, Asphalt Road and Driveways | 1353.0 m ² | 100.0% | ea | 1353.0 m ² |
| Existing Buildings, Asphalt Road and Driveways | 0.0 m ² | 100.0% | ea | 0.0 m ² |
| Landscape/Greenspace | 2513.7 m ² | 0.1% | ea | 2.5 m ² |
| TOTAL CATCHMENT IMPERVIOUS AREAS | | | | 1,356 m ² |
| TOTAL CATCHMENT AREA | | | | 3,867 m ² |
| EFFECTIVE WEIGHTED CATCHMENT % IMPERVIOUS RUNOFF COEFFICIENT | | | | 35.1 % 0.45 |

PROP - PROPOSED CONDITIONS

| A40 | <i>Footprint</i> | <i>% Impervious</i> | | <i>Effective Impervious Area</i> |
|---|-----------------------|---------------------|----|----------------------------------|
| Prop Buildings, Asphalt Road and Driveways | 1472.7 m ² | 100.0% | ea | 1472.7 m ² |
| Existing Buildings, Asphalt Road and Driveways | 0.0 m ² | 100.0% | ea | 0.0 m ² |
| Landscape/Greenspace | 2258.4 m ² | 0.1% | ea | 2.3 m ² |
| TOTAL CATCHMENT IMPERVIOUS AREAS | | | | 1,475 m ² |
| TOTAL CATCHMENT AREA | | | | 3,731 m ² |
| EFFECTIVE WEIGHTED CATCHMENT % IMPERVIOUS RUNOFF COEFFICIENT | | | | 39.5 % 0.48 |

PROP - PROPOSED CONDITIONS

| A50 | <i>Footprint</i> | <i>% Impervious</i> | | <i>Effective Impervious Area</i> |
|---|------------------------|---------------------|----|----------------------------------|
| Prop Buildings, Asphalt Road and Driveways | 233.1 m ² | 100.0% | ea | 233.1 m ² |
| Existing Buildings, Asphalt Road and Driveways | 1237.2 m ² | 100.0% | ea | 1237.2 m ² |
| Landscape/Greenspace | 12475.4 m ² | 0.1% | ea | 12.5 m ² |
| TOTAL CATCHMENT IMPERVIOUS AREAS | | | | 1,483 m ² |
| TOTAL CATCHMENT AREA | | | | 13,946 m ² |
| EFFECTIVE WEIGHTED CATCHMENT % IMPERVIOUS RUNOFF COEFFICIENT | | | | 10.6 % 0.27 |

| PROP - PROPOSED CONDITIONS | | | | |
|--|-------------------------|--------------|----|---------------------------|
| A60 | Footprint | % Impervious | | Effective Impervious Area |
| Prop Buildings, Asphalt Road and Driveways | 185.8 m ² | 100.0% | ea | 185.8 m ² |
| Existing Buildings, Asphalt Road and Driveways | 0.0 m ² | 100.0% | ea | 0.0 m ² |
| Landscape/Greenspace | 3340.5 m ² | 0.1% | ea | 3.3 m ² |
| TOTAL CATCHMENT IMPERVIOUS AREAS | | | | 189 m ² |
| TOTAL CATCHMENT AREA | | | | 3,526 m ² |
| EFFECTIVE WEIGHTED CATCHMENT % IMPERVIOUS RUNOFF COEFFICIENT | | | | 5.4 % 0.24 |
| PROP - PROPOSED CONDITIONS | | | | |
| A70 | Footprint | % Impervious | | Effective Impervious Area |
| Prop Buildings, Asphalt Road and Driveways | 236.7 m ² | 100.0% | ea | 236.7 m ² |
| Existing Buildings, Asphalt Road and Driveways | 0.0 m ² | 100.0% | ea | 0.0 m ² |
| Landscape/Greenspace | 3615.2 m ² | 0.1% | ea | 3.6 m ² |
| TOTAL CATCHMENT IMPERVIOUS AREAS | | | | 240 m ² |
| TOTAL CATCHMENT AREA | | | | 3,852 m ² |
| EFFECTIVE WEIGHTED CATCHMENT % IMPERVIOUS RUNOFF COEFFICIENT | | | | 6.2 % 0.24 |
| PROP - PROPOSED CONDITIONS | | | | |
| A80 | Footprint | % Impervious | | Effective Impervious Area |
| Prop Buildings, Asphalt Road and Driveways | 0.0 m ² | 100.0% | ea | 0.0 m ² |
| Existing Buildings, Asphalt Road and Driveways | 15364.5 m ² | 100.0% | ea | 15364.5 m ² |
| Landscape/Greenspace | 182319.6 m ² | 0.1% | ea | 182.3 m ² |
| TOTAL CATCHMENT IMPERVIOUS AREAS | | | | 15,547 m ² |
| TOTAL CATCHMENT AREA | | | | 197,684 m ² |
| EFFECTIVE WEIGHTED CATCHMENT % IMPERVIOUS RUNOFF COEFFICIENT | | | | 7.9 % 0.26 |

Stage Storage Discharge Calculations

DRY POND FACILITY

Project Name: JOSHUA COURT SUBDIVISON
 Project No.: 19126
 Date: March 2024

| Controlling Rim Elev: | | Pipe | DITCH VOLUME | DRY POND VOLUME | TOTAL VOLUME | Slot Weir Width (m) = 0.050 Invert (m) = 192.52 | Slot Weir Width (m) = 0.200 Invert (m) = 193.25 | Total Outflow |
|------------------------|-------------|-------------------|-------------------|-------------------|-------------------|---|---|---------------|
| Invert: | | 192.53 | | | | | | |
| Pipe Diameter: | | 0.610 | | | | | | |
| Structure/Pipe Length: | | 80.00 | | | | | | |
| | | | | | | | | DISCHARGE |
| Elevation (m) | | (m ³) | (m ³) | (m ³) | (m ³) | Slot Weir (m ³ /s) | Slot Weir (m ³ /s) | (m3/s) |
| 194 | 1.48 | 23.38 | 324.87 | 694.83 | 1043.08 | 0.166 | 0.239 | 0.405 |
| 193.9 | 1.38 | 23.38 | 263.45 | 629.99 | 916.82 | 0.149 | 0.193 | 0.342 |
| 193.8 | 1.28 | 23.38 | 210.3 | 562.24 | 795.92 | 0.133 | 0.150 | 0.283 |
| 193.7 | 1.18 | 23.38 | 164.84 | 500.51 | 688.73 | 0.118 | 0.111 | 0.229 |
| 193.6 | 1.08 | 23.38 | 126.46 | 441.72 | 591.56 | 0.103 | 0.076 | 0.179 |
| 193.5 | 0.98 | 23.38 | 94.56 | 385.81 | 503.75 | 0.089 | 0.046 | 0.135 |
| 193.4 | 0.88 | 23.38 | 68.54 | 332.69 | 424.61 | 0.076 | 0.021 | 0.097 |
| 193.3 | 0.78 | 23.38 | 47.79 | 282.31 | 353.48 | 0.063 | 0.004 | 0.067 |
| 193.2 | 0.68 | 23.38 | 31.73 | 234.58 | 289.69 | 0.052 | - | 0.052 |
| 193.1 | 0.58 | 22.73 | 19.75 | 189.44 | 231.92 | 0.041 | - | 0.041 |
| 193.06 | 0.54 | 21.57 | 15.98 | 172.1 | 209.65 | 0.037 | - | 0.037 |
| 193 | 0.48 | 19.33 | 11.28 | 146.82 | 177.43 | 0.031 | - | 0.031 |
| 192.9 | 0.38 | 14.84 | 5.66 | 106.63 | 127.13 | 0.022 | - | 0.022 |
| 192.8 | 0.28 | 9.99 | 2.32 | 68.81 | 81.12 | 0.014 | - | 0.014 |
| 192.7 | 0.18 | 5.32 | 0.66 | 33.29 | 39.27 | 0.007 | - | 0.007 |
| 192.6 | 0.08 | 1.49 | 0.08 | 0 | 1.57 | 0.002 | - | 0.002 |
| 192.52 | 0.00 | 0.00 | 0 | 0 | 0.00 | 0.000 | - | 0.000 |

| | | | | | | |
|--|---------------------------|--------------------------|--------------------------------------|--|--|--------------------------------------|
| Upper Canada Consultants 261 Martindale Road, Unit 1 St. Catharines, Ontario L2W 1A1 | | | | | | |
| MUNICIPALITY: | | TOWN OF WEST LINCOLN | | | | |
| PROJECT NAME: | | JOSHUA COURT SUBDIVISION | | | | |
| PROJECT NO.: | | 19126 | | | | |
| STORAGE AND OUTFLOW | | | | | | |
| DRY POND | | | | | | |
| Elevation (m) | Increment Depth (m) | Active Depth (m) | Surface Area (m ²) | Average Surface Area (m ²) | Increment Volume (m ³) | Total Volume (m ³) |
| 192.60 | | 0.00 | 322.00 | | | 0.0 |
| | 0.10 | | | 332.95 | 33.29 | |
| 192.70 | | 0.10 | 343.89 | | | 33.29 |
| | 0.10 | | | 355.20 | 35.52 | |
| 192.80 | | 0.20 | 366.51 | | | 68.81 |
| | 0.10 | | | 378.17 | 37.82 | |
| 192.90 | | 0.30 | 389.84 | | | 106.63 |
| | 0.10 | | | 401.87 | 40.19 | |
| 193.00 | | 0.40 | 413.89 | | | 146.82 |
| | 0.06 | | | 421.28 | 25.28 | |
| 193.06 | | 0.46 | 428.67 | | | 172.10 |
| | 0.04 | | | 433.67 | 17.35 | |
| 193.10 | | 0.50 | 438.67 | | | 189.44 |
| | 0.10 | | | 451.41 | 45.14 | |
| 193.20 | | 0.60 | 464.16 | | | 234.58 |
| | 0.10 | | | 477.27 | 47.73 | |
| 193.30 | | 0.70 | 490.37 | | | 282.31 |
| | 0.10 | | | 503.84 | 50.38 | |
| 193.4 | | 0.80 | 517.31 | | | 332.69 |
| | 0.10 | | | 531.13 | 53.11 | |
| 193.5 | | 0.90 | 544.96 | | | 385.81 |
| | 0.10 | | | 559.15 | 55.91 | |
| 193.6 | | 1.00 | 573.33 | | | 441.72 |
| | 0.10 | | | 587.88 | 58.79 | |
| 193.7 | | 1.10 | 602.43 | | | 500.51 |
| | 0.10 | | | 617.33 | 61.73 | |
| 193.8 | | 1.20 | 632.24 | | | 562.24 |
| | 0.10 | | | 647.51 | 64.75 | |
| 193.9 | | 1.30 | 662.77 | | | 626.99 |
| | 0.10 | | | 678.40 | 67.84 | |
| 194 | | 1.40 | 694.03 | | | 694.83 |

| Upper Canada Consultants 261 Martindale Road, Unit 1 St. Catharines, Ontario L2W 1A1 | | | | | | |
|--|---------------------------|------------------------|--|--|--|--------------------------------------|
| MUNICIPALITY: TOWNSHIP OF WEST LINCOLN PROJECT NAME: JOSHUA COURT SUBDIVISION PROJECT NO.: 19126 | | | | | | |
| STORAGE AND OUTFLOW | | | | | | |
| <u>A20 1% Ditch Storage: Calculation is per ditch</u> | | | | | | |
| Elevation (m) | Increment Depth (m) | Active Depth (m) | Cross-Section Area (m ²) | Average Cross-Section Area (m ²) | Increment Volume (m ³) | Total Volume (m ³) |
| 192.52 | | 0.00 | 0.00 | | | 0.0 |
| | 0.08 | 0.08 | 0.02 | 0.010 | 0.08 | 0.08 |
| 192.60 | | 0.08 | 0.02 | 0.058 | 0.58 | 0.66 |
| | 0.10 | 0.18 | 0.10 | 0.166 | 1.66 | 2.32 |
| 192.70 | | 0.28 | 0.24 | 0.334 | 3.34 | 5.66 |
| | 0.10 | 0.38 | 0.43 | 0.562 | 5.62 | 11.28 |
| 192.80 | | 0.48 | 0.69 | 0.783 | 4.70 | 15.98 |
| | 0.06 | 0.54 | 0.87 | 0.942 | 3.77 | 19.75 |
| 192.90 | | 0.58 | 1.01 | 1.198 | 11.98 | 31.73 |
| | 0.10 | 0.68 | 1.39 | 1.606 | 16.06 | 47.79 |
| 193.00 | | 0.78 | 1.83 | 2.074 | 20.74 | 68.54 |
| | 0.10 | 0.88 | 2.32 | 2.602 | 26.02 | 94.56 |
| 193.06 | | 0.98 | 2.88 | 3.190 | 31.90 | 126.46 |
| | 0.10 | 1.08 | 3.50 | 3.838 | 38.38 | 164.84 |
| 193.10 | | 1.18 | 4.18 | 4.546 | 45.46 | 210.30 |
| | 0.10 | 1.28 | 4.92 | 5.314 | 53.14 | 263.45 |
| 193.20 | | 1.38 | 5.71 | 6.142 | 61.42 | 324.87 |
| | 0.10 | 1.48 | 6.57 | | | |
| 193.30 | | | | | | |
| | | | | | | |
| 193.40 | | | | | | |
| | | | | | | |
| 193.50 | | | | | | |
| | | | | | | |
| 193.60 | | | | | | |
| | | | | | | |
| 193.70 | | | | | | |
| | | | | | | |
| 193.80 | | | | | | |
| | | | | | | |
| 193.90 | | | | | | |
| | | | | | | |
| 194.00 | | | | | | |

APPENDIX B

MIDUSS Output Files – Overall Stormwater Management Plan Calculations

Stormwater Management Plan

Joshua Court Subdivision – Township of West Lincoln

Existing Conditions

Output File (4.7) EX.OUT opened 2024-03-06 16:16
Units used are defined by G = 9.810
24 144 10.000 are MAXDT MAXHYD & DTMIN values
Licensee: UPPER CANADA CONSULTANTS
COMMENT
3 line(s) of comment
ALAN CORNERS SUBDIVISION, WEST LINCOLN
STORMWATER MANAGEMENT PLAN
EXISTING CONDITIONS
14 START
1 1=Zero; 2=Define
35 COMMENT
3 line(s) of comment

5 YEAR DESIGN STORM EVENT

2 STORM
1 1=Chicago;2=Huff;3=User;4=Cdnlhr;5=Historic
3175.000 Coefficient a
20.000 Constant b (min)
1.000 Exponent c
.450 Fraction to peak r
240.000 Duration o 240 min
48.843 mm Total depth
3 IMPERVIOUS
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.015 Manning "n"
98.000 SCS Curve No or C
.100 Ia/S Coefficient
.518 Initial Abstraction
35 COMMENT
3 line(s) of comment
*
OUTLET A
*
4 CATCHMENT
2.000 ID No.6 99999
.420 Area in hectares
52.915 Length (PERV) metres
.500 Gradient (%)
42.600 Per cent Impervious
52.915 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
74.000 SCS Curve No or C
.100 Ia/S Coefficient
8.924 Initial Abstraction
1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
.040 .000 .000 .000 c.m/s
.252 .877 .518 C perv/imperv/total
15 ADD RUNOFF
.040 .040 .000 .000 c.m/s
14 START
1 1=Zero; 2=Define
35 COMMENT
3 line(s) of comment
*
OUTLET B
*
4 CATCHMENT
4.000 ID No.6 99999
2.290 Area in hectares
123.558 Length (PERV) metres
.500 Gradient (%)
3.800 Per cent Impervious
123.558 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
74.000 SCS Curve No or C
.100 Ia/S Coefficient
8.924 Initial Abstraction
1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
.040 .000 .000 .000 c.m/s
.253 .876 .276 C perv/imperv/total
15 ADD RUNOFF
.040 .040 .000 .000 c.m/s
9 ROUTE
.000 Conduit Length
.000 No Conduit defined
.000 Zero lag
.000 Beta weighting factor
.000 Routing timestep
0 No. of sub-reaches
.040 .040 .040 .000 c.m/s
17 COMBINE
1 Junction Node No.
.040 .040 .040 .040 c.m/s
14 START
1 1=Zero; 2=Define
35 COMMENT
3 line(s) of comment
*
OUTLET D
*
4 CATCHMENT
1.000 ID No.6 99999
19.770 Area in hectares
363.043 Length (PERV) metres
.500 Gradient (%)
7.900 Per cent Impervious
363.043 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
74.000 SCS Curve No or C
.100 Ia/S Coefficient
8.924 Initial Abstraction
1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
.340 .000 .040 .040 c.m/s
.253 .889 .303 C perv/imperv/total
15 ADD RUNOFF
.340 .340 .040 .040 c.m/s
35 COMMENT

3 line(s) of comment
*
OUTLET C
*
4 CATCHMENT
3.000 ID No.6 99999
2.230 Area in hectares
121.929 Length (PERV) metres
.500 Gradient (%)
5.600 Per cent Impervious
121.929 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
74.000 SCS Curve No or C
.100 Ia/S Coefficient
8.924 Initial Abstraction
1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
.040 .340 .040 .040 c.m/s
.253 .876 .287 C perv/imperv/total
15 ADD RUNOFF
.040 .375 .040 .040 c.m/s
9 ROUTE
.000 Conduit Length
.000 No Conduit defined
.000 Zero lag
.000 Beta weighting factor
.000 Routing timestep
0 No. of sub-reaches
.040 .375 .375 .040 c.m/s
17 COMBINE
1 Junction Node No.
.040 .375 .375 .402 c.m/s
18 CONFLUENCE
1 Junction Node No.
.040 .402 .375 .000 c.m/s
14 START
1 1=Zero; 2=Define
35 COMMENT
3 line(s) of comment

100 YEAR DESIGN STORM EVENT

2 STORM
1 1=Chicago;2=Huff;3=User;4=Cdnlhr;5=Historic
6300.000 Coefficient a
15.000 Constant b (min)
1.000 Exponent c
.450 Fraction to peak r
240.000 Duration o 240 min
98.819 mm Total depth
3 IMPERVIOUS
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.015 Manning "n"
98.000 SCS Curve No or C
.100 Ia/S Coefficient
.518 Initial Abstraction
35 COMMENT
3 line(s) of comment
*
OUTLET A
*
4 CATCHMENT
2.000 ID No.6 99999
.420 Area in hectares
52.915 Length (PERV) metres
.500 Gradient (%)
42.600 Per cent Impervious
52.915 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
74.000 SCS Curve No or C
.100 Ia/S Coefficient
8.924 Initial Abstraction
1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
.109 .000 .375 .000 c.m/s
.456 .933 .659 C perv/imperv/total
15 ADD RUNOFF
.109 .109 .375 .000 c.m/s
14 START
1 1=Zero; 2=Define
35 COMMENT
3 line(s) of comment
*
OUTLET B
*
4 CATCHMENT
4.000 ID No.6 99999
2.290 Area in hectares
123.558 Length (PERV) metres
.500 Gradient (%)
3.800 Per cent Impervious
123.558 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
74.000 SCS Curve No or C
.100 Ia/S Coefficient
8.924 Initial Abstraction
1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
.245 .000 .375 .000 c.m/s
.455 .931 .473 C perv/imperv/total
15 ADD RUNOFF
.245 .245 .375 .000 c.m/s
9 ROUTE
.000 Conduit Length
.000 No Conduit defined
.000 Zero lag
.000 Beta weighting factor
.000 Routing timestep
0 No. of sub-reaches
.245 .245 .245 .000 c.m/s
17 COMBINE
1 Junction Node No.
.245 .245 .245 .245 c.m/s
14 START

Stormwater Management Plan

Joshua Court Subdivision – Township of West Lincoln

| | | | | |
|------------|--|---------|--|---------------------|
| 1 | 1=Zero; 2=Define | 5.600 | Per cent Impervious | |
| 35 | COMMENT | 121.929 | Length (IMPERV) | |
| 3 | line(s) of comment | .000 | %Imp. with Zero Dpth | |
| * | | 1 | Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat | |
| | OUTLET D | .250 | Manning "n" | |
| * | | 74.000 | SCS Curve No or C | |
| 4 | CATCHMENT | .100 | Ia/S Coefficient | |
| 1.000 | ID No.6 99999 | 8.924 | Initial Abstraction | |
| 19.770 | Area in hectares | 1 | Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv | |
| 363.043 | Length (PERV) metres | .239 | 1.270 | .245 |
| .500 | Gradient (%) | .455 | .931 | .482 |
| 7.900 | Per cent Impervious | | | C perv/imperv/total |
| 363.043 | Length (IMPERV) | 15 | ADD RUNOFF | |
| .000 | %Imp. with Zero Dpth | .239 | 1.450 | .245 |
| 1 | Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat | | | .245 c.m/s |
| .250 | Manning "n" | 9 | ROUTE | |
| 74.000 | SCS Curve No or C | .000 | Conduit Length | |
| .100 | Ia/S Coefficient | .000 | No Conduit defined | |
| 8.924 | Initial Abstraction | .000 | Zero lag | |
| 1 | Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv | .000 | Beta weighting factor | |
| 1.270 | .000 | .000 | Routing timestep | |
| .456 | .944 | 0 | No. of sub-reaches | |
| .495 | | .239 | 1.450 | 1.450 |
| | C perv/imperv/total | | | .245 c.m/s |
| 15 | ADD RUNOFF | 17 | COMBINE | |
| 1.270 | 1.270 | 1 | Junction Node No. | |
| .245 | | .239 | 1.450 | 1.450 |
| .245 c.m/s | | | | 1.649 c.m/s |
| 35 | COMMENT | 18 | CONFLUENCE | |
| 3 | line(s) of comment | 1 | Junction Node No. | |
| * | | .239 | 1.649 | 1.450 |
| | OUTLET C | | | .000 c.m/s |
| * | | 20 | MANUAL | |
| 4 | CATCHMENT | | | |
| 3.000 | ID No.6 99999 | | | |
| 2.230 | Area in hectares | | | |
| 121.929 | Length (PERV) metres | | | |
| .500 | Gradient (%) | | | |

Developed Conditions – NO SWM

Upper Canada Consultants

Stormwater Management Plan

Joshua Court Subdivision, Township of West Lincoln

| | | | | | | |
|-----------------------------|--|---------------------|------------|---------|--|---------------------|
| 17 | COMBINE | | | | 98.000 | SCS Curve No or C |
| 2 | Junction Node No. | | | | .100 | Ia/S Coefficient |
| | .340 .340 | .340 | .340 c.m/s | | .518 | Initial Abstraction |
| 14 | START | | | 35 | COMMENT | |
| 1 | 1=Zero; 2=Define | | | 3 | line(s) of comment | |
| 4 | CATCHMENT | | | * | OUTLET A | |
| 50.000 | ID No.6 99999 | | | 4 | CATCHMENT | |
| 1.390 | Area in hectares | | | 10.000 | ID No.6 99999 | |
| 92.263 | Length (PERV) metres | | | .450 | Area in hectares | |
| 1.000 | Gradient (%) | | | 54.772 | Length (PERV) metres | |
| 10.600 | Per cent Impervious | | | .500 | Gradient (%) | |
| 92.263 | Length (IMPERV) | | | 40.700 | Per cent Impervious | |
| .000 | %Imp. with Zero Dpth | | | 54.772 | Length (IMPERV) | |
| 1 | Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat | | | .000 | %Imp. with Zero Dpth | |
| .250 | Manning "n" | | | 1 | Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat | |
| 74.000 | SCS Curve No or C | | | .250 | Manning "n" | |
| .100 | Ia/S Coefficient | | | 74.000 | SCS Curve No or C | |
| 8.924 | Initial Abstraction | | | .100 | Ia/S Coefficient | |
| 1 | Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv | | | 8.924 | Initial Abstraction | |
| .037 | .000 .340 | .340 c.m/s | | 1 | Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv | |
| .252 | .876 .318 | C perv/imperv/total | | .112 | .000 .385 | .000 c.m/s |
| 15 | ADD RUNOFF | | | .455 | .933 .649 | C perv/imperv/total |
| .037 | .037 .340 | .340 c.m/s | | 15 | ADD RUNOFF | |
| 9 | ROUTE | | | .112 | .112 .385 | .000 c.m/s |
| .000 | Conduit Length | | | 14 | START | |
| .000 | No Conduit defined | | | 1 | 1=Zero; 2=Define | |
| .000 | Zero lag | | | 35 | COMMENT | |
| .000 | Beta weighting factor | | | 3 | line(s) of comment | |
| .000 | Routing timestep | | | * | OUTLET B | |
| 0 | No. of sub-reaches | | | 4 | CATCHMENT | |
| .037 | .037 .037 | .340 c.m/s | | 20.000 | ID No.6 99999 | |
| 17 | COMBINE | | | 1.590 | Area in hectares | |
| 2 | Junction Node No. | | | 102.956 | Length (PERV) metres | |
| .037 | .037 .037 | .377 c.m/s | | 1.000 | Gradient (%) | |
| 14 | START | | | 7.500 | Per cent Impervious | |
| 1 | 1=Zero; 2=Define | | | 102.307 | Length (IMPERV) | |
| 4 | CATCHMENT | | | .000 | %Imp. with Zero Dpth | |
| 60.000 | ID No.6 99999 | | | 1 | Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat | |
| .360 | Area in hectares | | | .250 | Manning "n" | |
| 48.990 | Length (PERV) metres | | | 74.000 | SCS Curve No or C | |
| 1.000 | Gradient (%) | | | .100 | Ia/S Coefficient | |
| 5.400 | Per cent Impervious | | | 8.924 | Initial Abstraction | |
| 46.990 | Length (IMPERV) | | | 1 | Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv | |
| .000 | %Imp. with Zero Dpth | | | .221 | .000 .385 | .000 c.m/s |
| 1 | Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat | | | .456 | .934 .492 | C perv/imperv/total |
| .250 | Manning "n" | | | 15 | ADD RUNOFF | |
| 74.000 | SCS Curve No or C | | | .221 | .221 .385 | .000 c.m/s |
| .100 | Ia/S Coefficient | | | 9 | ROUTE | |
| 8.924 | Initial Abstraction | | | .000 | Conduit Length | |
| 1 | Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv | | | .000 | No Conduit defined | |
| .011 | .000 .037 | .377 c.m/s | | .000 | Zero lag | |
| .252 | .883 .286 | C perv/imperv/total | | .000 | Beta weighting factor | |
| 15 | ADD RUNOFF | | | .000 | Routing timestep | |
| .011 | .011 .037 | .377 c.m/s | | 0 | No. of sub-reaches | |
| 9 | ROUTE | | | .221 | .221 .221 | .000 c.m/s |
| .000 | Conduit Length | | | 17 | COMBINE | |
| .000 | No Conduit defined | | | 1 | Junction Node No. | |
| .000 | Zero lag | | | .221 | .221 .221 | .221 c.m/s |
| .000 | Beta weighting factor | | | 14 | START | |
| .000 | Routing timestep | | | 1 | 1=Zero; 2=Define | |
| 0 | No. of sub-reaches | | | 4 | CATCHMENT | |
| .011 | .011 .011 | .377 c.m/s | | 30.000 | ID No.6 99999 | |
| 17 | COMBINE | | | .390 | Area in hectares | |
| 2 | Junction Node No. | | | 50.990 | Length (PERV) metres | |
| .011 | .011 .011 | .385 c.m/s | | .500 | Gradient (%) | |
| 14 | START | | | 35.100 | Per cent Impervious | |
| 1 | 1=Zero; 2=Define | | | 50.990 | Length (IMPERV) | |
| 9 | ROUTE | | | .000 | %Imp. with Zero Dpth | |
| .000 | Conduit Length | | | 1 | Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat | |
| .000 | No Conduit defined | | | .250 | Manning "n" | |
| .000 | Zero lag | | | 74.000 | SCS Curve No or C | |
| .000 | Beta weighting factor | | | .100 | Ia/S Coefficient | |
| .000 | Routing timestep | | | 8.924 | Initial Abstraction | |
| 0 | No. of sub-reaches | | | 1 | Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv | |
| .011 | .000 .000 | .385 c.m/s | | .086 | .000 .221 | .221 c.m/s |
| 18 | CONFLUENCE | | | .456 | .933 .623 | C perv/imperv/total |
| 2 | Junction Node No. | | | 15 | ADD RUNOFF | |
| .011 | .385 .000 | .000 c.m/s | | .086 | .086 .221 | .221 c.m/s |
| 9 | ROUTE | | | 9 | ROUTE | |
| .000 | Conduit Length | | | .000 | Conduit Length | |
| .000 | No Conduit defined | | | .000 | No Conduit defined | |
| .000 | Zero lag | | | .000 | Zero lag | |
| .000 | Beta weighting factor | | | .000 | Beta weighting factor | |
| .000 | Routing timestep | | | 0 | Routing timestep | |
| 0 | No. of sub-reaches | | | .086 | .086 .086 | .221 c.m/s |
| .011 | .385 .385 | .000 c.m/s | | 17 | COMBINE | |
| 17 | COMBINE | | | 1 | Junction Node No. | |
| 3 | Junction Node No. | | | .086 | .086 .086 | .280 c.m/s |
| .011 | .385 .385 | .481 c.m/s | | 14 | START | |
| 14 | START | | | 1 | 1=Zero; 2=Define | |
| 1 | 1=Zero; 2=Define | | | 4 | CATCHMENT | |
| 35 | COMMENT | | | 40.000 | ID No.6 99999 | |
| 3 | line(s) of comment | | | .370 | Area in hectares | |
| * | OUTLET E | | | 49.665 | Length (PERV) metres | |
| * | | | | .500 | Gradient (%) | |
| 18 | CONFLUENCE | | | 39.500 | Per cent Impervious | |
| 3 | Junction Node No. | | | 49.665 | Length (IMPERV) | |
| .011 | .481 .385 | .000 c.m/s | | .000 | %Imp. with Zero Dpth | |
| 14 | START | | | 1 | Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat | |
| 1 | 1=Zero; 2=Define | | | .250 | Manning "n" | |
| 35 | COMMENT | | | 74.000 | SCS Curve No or C | |
| 3 | line(s) of comment | | | .100 | Ia/S Coefficient | |
| ***** | ***** | | | 8.924 | Initial Abstraction | |
| 100 YEAR DESIGN STORM EVENT | | | | 1 | Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv | |
| ***** | | | | .091 | .000 .086 | .280 c.m/s |
| 2 | STORM | | | .456 | .932 .644 | C perv/imperv/total |
| 1 | 1=Chicago; 2=Huff; 3=User; 4=Cdnlhr; 5=Historic | | | 15 | ADD RUNOFF | |
| 6300.000 | Coefficient a | | | .091 | .091 .086 | .280 c.m/s |
| 15.000 | Constant b (min) | | | 9 | ROUTE | |
| 1.000 | Exponent c | | | .000 | Conduit Length | |
| .450 | Fraction to peak r | | | .000 | No Conduit defined | |
| 240.000 | Duration 0 240 min | | | .000 | Zero lag | |
| 98.819 mm | Total depth | | | | | |
| 3 | IMPERVIOUS | | | | | |
| 1 | Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat | | | | | |
| .015 | Manning "n" | | | | | |

Stormwater Management Plan

Joshua Court Subdivision, Township of West Lincoln

| | | | | | | | | | |
|---------|--|--|---------------------|---------------------|-------------|--|----------------|---------------------|-------------|
| | .000 | Beta weighting factor | | | | .200 | .200 | .200 | 1.270 c.m/s |
| | .000 | Routing timestep | | | 17 | COMBINE | | | |
| | 0 | No. of sub-reaches | | | 2 | Junction Node No. | .200 | .200 | 1.342 c.m/s |
| 17 | .091 | .091 | .091 | .280 c.m/s | | | | | |
| | COMBINE | | | | 14 | START | | | |
| | 1 | Junction Node No. | | | 1 | 1=Zero; 2=Define | | | |
| 14 | .091 | .091 | .091 | .339 c.m/s | 4 | CATCHMENT | | | |
| | 1 | 1=Zero; 2=Define | | | 60.000 | ID No.6 99999 | | | |
| 4 | CATCHMENT | | | | .360 | Area in hectares | | | |
| | 70.000 | ID No.6 99999 | | | 48.990 | Length (PERV) metres | | | |
| | .390 | Area in hectares | | | 1.000 | Gradient (%) | | | |
| 50.990 | Length (PERV) metres | | | | 5.400 | Per cent Impervious | | | |
| .500 | Gradient (%) | | | | 46.990 | Length (IMPERV) | | | |
| 6.200 | Per cent Impervious | | | | .000 | %Imp. with Zero Dpth | | | |
| 50.990 | Length (IMPERV) | | | | 1 | Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat | | | |
| .000 | %Imp. with Zero Dpth | | | | .250 | Manning "n" | | | |
| 1 | Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat | | | | 74.000 | SCS Curve No or C | | | |
| .250 | Manning "n" | | | | .100 | Ia/S Coefficient | | | |
| 74.000 | SCS Curve No or C | | | | 8.924 | Initial Abstraction | | | |
| .100 | Ia/S Coefficient | | | | 1 | Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv | | | |
| 8.924 | Initial Abstraction | | | | .062 | .000 | .200 | 1.342 c.m/s | |
| 1 | Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv | | | | .456 | .923 | .480 | C perv/imperv/total | |
| .059 | .000 | .091 | .339 c.m/s | 15 | ADD RUNOFF | .062 | .062 | .200 | 1.342 c.m/s |
| .456 | .933 | .486 | C perv/imperv/total | 9 | ROUTE | | | | |
| .059 | .059 | .091 | .339 c.m/s | | .000 | Conduit Length | | | |
| 9 | ROUTE | | | | .000 | No Conduit defined | | | |
| | .000 | Conduit Length | | | .000 | Zero lag | | | |
| | .000 | No Conduit defined | | | .000 | Beta weighting factor | | | |
| | .000 | Zero lag | | | .000 | Routing timestep | | | |
| | .000 | Beta weighting factor | | | 0 | No. of sub-reaches | .062 | .062 | 1.342 c.m/s |
| | .000 | Routing timestep | | | 17 | COMBINE | | | |
| | 0 | No. of sub-reaches | | | 2 | Junction Node No. | .062 | .062 | 1.357 c.m/s |
| 17 | .059 | .059 | .059 | .339 c.m/s | 14 | START | | | |
| | COMBINE | | | | 1 | 1=Zero; 2=Define | | | |
| | 1 | Junction Node No. | | | 9 | ROUTE | | | |
| 14 | .059 | .059 | .059 | .395 c.m/s | | .000 | Conduit Length | | |
| | 1 | 1=Zero; 2=Define | | | .000 | No Conduit defined | | | |
| 18 | CONFLUENCE | | | | .000 | Zero lag | | | |
| | 1 | Junction Node No. | | | .000 | Beta weighting factor | | | |
| 9 | .059 | .395 | .059 | .000 c.m/s | .000 | Routing timestep | | | |
| | ROUTE | | | | 0 | No. of sub-reaches | .062 | .000 | 1.357 c.m/s |
| | .000 | Conduit Length | | | 18 | CONFLUENCE | | | |
| | .000 | No Conduit defined | | | 2 | Junction Node No. | .062 | 1.357 | .000 c.m/s |
| | .000 | Zero lag | | | 9 | ROUTE | | | |
| | .000 | Beta weighting factor | | | .000 | Conduit Length | | | |
| | .000 | Routing timestep | | | .000 | No Conduit defined | | | |
| | 0 | No. of sub-reaches | .395 | .000 c.m/s | .000 | Zero lag | | | |
| 17 | .059 | .395 | .395 | .395 c.m/s | .000 | Beta weighting factor | | | |
| | COMBINE | | | | .000 | Routing timestep | | | |
| | 3 | Junction Node No. | | | 0 | No. of sub-reaches | .062 | 1.357 | 1.357 |
| 14 | .059 | .395 | .395 | .395 c.m/s | 17 | COMBINE | | | |
| | 1 | 1=Zero; 2=Define | | | 3 | Junction Node No. | .062 | 1.357 | 1.357 |
| 35 | COMMENT | | | | 14 | START | | | |
| | 3 | line(s) of comment | | | 1 | 1=Zero; 2=Define | | | |
| | * OUTLET C | | | | 35 | COMMENT | | | |
| | * OUTLET E | | | | 3 | line(s) of comment | | | |
| 4 | CATCHMENT | | | | * OUTLET E | | | | |
| | 80.000 | ID No.6 99999 | | | 18 | CONFLUENCE | | | |
| | 19.770 | Area in hectares | | | 3 | Junction Node No. | .062 | 1.717 | 1.357 |
| 363.043 | Length (PERV) metres | | | | .062 | 1.717 | 1.357 | .000 c.m/s | |
| .500 | Gradient (%) | | | | 20 | MANUAL | | | |
| 7.900 | Per cent Impervious | | | | | | | | |
| 363.043 | Length (IMPERV) | | | | | | | | |
| .000 | %Imp. with Zero Dpth | | | | | | | | |
| 1 | Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat | | | | | | | | |
| .250 | Manning "n" | | | | | | | | |
| 74.000 | SCS Curve No or C | | | | | | | | |
| .100 | Ia/S Coefficient | | | | | | | | |
| 8.924 | Initial Abstraction | | | | | | | | |
| 1 | Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv | | | | | | | | |
| 1.270 | .000 | .395 | .395 c.m/s | | | | | | |
| .456 | .944 | .495 | C perv/imperv/total | | | | | | |
| 15 | ADD RUNOFF | 1.270 | 1.270 | .395 | .395 c.m/s | | | | |
| | ROUTE | | | | | | | | |
| | .000 | Conduit Length | | | | | | | |
| | .000 | No Conduit defined | | | | | | | |
| | .000 | Zero lag | | | | | | | |
| | .000 | Beta weighting factor | | | | | | | |
| | .000 | Routing timestep | | | | | | | |
| | 0 | No. of sub-reaches | 1.270 | .395 c.m/s | | | | | |
| 17 | COMBINE | | | | | | | | |
| | 2 | Junction Node No. | 1.270 | 1.270 | 1.270 c.m/s | | | | |
| 14 | START | | | | | | | | |
| | 1 | 1=Zero; 2=Define | | | | | | | |
| 4 | CATCHMENT | | | | | | | | |
| | 50.000 | ID No.6 99999 | | | | | | | |
| | 1.390 | Area in hectares | | | | | | | |
| | 92.263 | Length (PERV) metres | | | | | | | |
| | 1.000 | Gradient (%) | | | | | | | |
| | 10.600 | Per cent Impervious | | | | | | | |
| | 92.263 | Length (IMPERV) | | | | | | | |
| | .000 | %Imp. with Zero Dpth | | | | | | | |
| | 1 | Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat | | | | | | | |
| | .250 | Manning "n" | | | | | | | |
| | 74.000 | SCS Curve No or C | | | | | | | |
| | .100 | Ia/S Coefficient | | | | | | | |
| | 8.924 | Initial Abstraction | | | | | | | |
| | 1 | Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv | | | | | | | |
| | .200 | .000 | 1.270 | 1.270 c.m/s | | | | | |
| | .454 | .935 | .505 | C perv/imperv/total | | | | | |
| 15 | ADD RUNOFF | .200 | .200 | 1.270 | 1.270 c.m/s | | | | |
| | ROUTE | | | | | | | | |
| | .000 | Conduit Length | | | | | | | |
| | .000 | No Conduit defined | | | | | | | |
| | .000 | Zero lag | | | | | | | |
| | .000 | Beta weighting factor | | | | | | | |
| | .000 | Routing timestep | | | | | | | |
| | 0 | No. of sub-reaches | | | | | | | |

Stormwater Management Plan

Joshua Court Subdivision, Township of West Lincoln

Developed Conditions – FULL SWM

Output File (4.7) SWM.OUT opened 2024-03-12 16:40
Units used are defined by G = 9.810
24 144 10.000 are MAXDT MAXHYD & DTMIN values

Licensee: UPPER CANADA CONSULTANTS

COMMENT

3 line(s) of comment
ALAN CORNERS SUBDIVISION, WEST LINCOLN
STORMWATER MANAGEMENT PLAN
EXISTING CONDITIONS

35 COMMENT

3 line(s) of comment

25mm MOEE DESIGN STORM

2 STORM

1 l=Chicago;2=Huff;3=User;4=Cdnlhr;5=Historic
512.000 Coefficient a
6.000 Constant b (min)
.800 Exponent c
.450 Fraction to peak r
240.000 Duration ó 240 min
25.035 mm Total depth

3 IMPERVIOUS

1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.015 Manning "n"
98.000 SCS Curve No or C
.100 Ia/S Coefficient
.518 Initial Abstraction

14 START

1 l=Zero; 2=Define

4 CATCHMENT

30.000 ID No.ó 99999
.390 Area in hectares
50.990 Length (PERV) metres
.500 Gradient (%)
35.100 Per cent Impervious
50.990 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
74.000 SCS Curve No or C
.100 Ia/S Coefficient
8.924 Initial Abstraction

1 Option 1=Trianglrr; 2=Rectanglrr; 3=SWM HYD; 4=Lin. Reserv
.012 .000 .000 c.m/s
.098 .796 .343 C perv/imperv/total

15 ADD RUNOFF

.012 .012 .000 .000 c.m/s

11 CHANNEL

.100 Base Width =
3.000 Left bank slope 1:
3.000 Right bank slope 1:
.040 Manning's "n"
.500 O/a Depth in metres
.500 Select Grade in %
Depth = .108 metres
Velocity = .266 m/sec
Flow Capacity = .554 c.m/s
Critical depth = .066 metres

9 ROUTE

110.000 Conduit Length
.458 Supply X-factor <.5
309.776 Supply K-lag (sec)
.500 Beta weighting factor
300.000 Routing timestep
1 No. of sub-reaches
.012 .012 .012 .000 c.m/s

14 START

1 l=Zero; 2=Define

4 CATCHMENT

40.000 ID No.ó 99999
.370 Area in hectares
49.665 Length (PERV) metres
.500 Gradient (%)
39.500 Per cent Impervious
49.665 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
74.000 SCS Curve No or C
.100 Ia/S Coefficient
8.924 Initial Abstraction

1 Option 1=Trianglrr; 2=Rectanglrr; 3=SWM HYD; 4=Lin. Reserv
.013 .000 .012 .000 c.m/s
.098 .797 .374 C perv/imperv/total

15 ADD RUNOFF

.013 .013 .012 .000 c.m/s

11 CHANNEL

.100 Base Width =
3.000 Left bank slope 1:
3.000 Right bank slope 1:
.040 Manning's "n"
.600 O/a Depth in metres
.500 Select Grade in %
Depth = .111 metres
Velocity = .271 m/sec
Flow Capacity = .888 c.m/s
Critical depth = .068 metres

9 ROUTE

76.000 Conduit Length
.438 Supply X-factor <.5
210.169 Supply K-lag (sec)
.500 Beta weighting factor
200.000 Routing timestep
1 No. of sub-reaches
.013 .013 .013 .000 c.m/s

14 START

1 l=Zero; 2=Define

35 COMMENT

3 line(s) of comment

5 YEAR DESIGN STORM EVENT

2 STORM

1 l=Chicago;2=Huff;3=User;4=Cdnlhr;5=Historic
3175.000 Coefficient a
20.000 Constant b (min)
1.000 Exponent c
.450 Fraction to peak r
240.000 Duration ó 240 min
48.843 mm Total depth

3 IMPERVIOUS

1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.015 Manning "n"
98.000 SCS Curve No or C
.100 Ia/S Coefficient
.518 Initial Abstraction

35 COMMENT

3 line(s) of comment

* OUTLET B

* CATCHMENT

30.000 ID No.ó 99999
.390 Area in hectares
50.990 Length (PERV) metres
.500 Gradient (%)
35.100 Per cent Impervious
50.990 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
74.000 SCS Curve No or C
.100 Ia/S Coefficient
8.924 Initial Abstraction
1 Option 1=Trianglrr; 2=Rectanglrr; 3=SWM HYD; 4=Lin. Reserv
.031 .000 .013 .000 c.m/s
.252 .878 .472 C perv/imperv/total

15 ADD RUNOFF

.031 .031 .013 .000 c.m/s

11 CHANNEL

.100 Base Width =
3.000 Left bank slope 1:
3.000 Right bank slope 1:
.040 Manning's "n"
.500 O/a Depth in metres
.500 Select Grade in %
Depth = .159 metres
Velocity = .336 m/sec
Flow Capacity = .554 c.m/s
Critical depth = .101 metres

9 ROUTE

110.000 Conduit Length
.441 Supply X-factor <.5
245.520 Supply K-lag (sec)
.500 Beta weighting factor
200.000 Routing timestep
1 No. of sub-reaches
.031 .031 .028 .000 c.m/s

17 COMBINE

1 Junction Node No.

.031 .031 .028 .028 c.m/s

14 START

1 l=Zero; 2=Define

4 CATCHMENT

40.000 ID No.ó 99999
.370 Area in hectares
49.665 Length (PERV) metres
.500 Gradient (%)
39.500 Per cent Impervious
49.665 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
74.000 SCS Curve No or C
.100 Ia/S Coefficient
8.924 Initial Abstraction

1 Option 1=Trianglrr; 2=Rectanglrr; 3=SWM HYD; 4=Lin. Reserv
.033 .000 .028 .028 c.m/s
.252 .879 .500 C perv/imperv/total

15 ADD RUNOFF

.033 .033 .028 .028 c.m/s

11 CHANNEL

.100 Base Width =
3.000 Left bank slope 1:
3.000 Right bank slope 1:
.040 Manning's "n"
.600 O/a Depth in metres
.500 Select Grade in %
Depth = .163 metres
Velocity = .342 m/sec
Flow Capacity = .888 c.m/s
Critical depth = .104 metres

9 ROUTE

76.000 Conduit Length
.412 Supply X-factor <.5
166.890 Supply K-lag (sec)
.500 Beta weighting factor
150.000 Routing timestep
1 No. of sub-reaches
.033 .033 .029 .028 c.m/s

17 COMBINE

1 Junction Node No.

.033 .033 .029 .057 c.m/s

14 START

1 l=Zero; 2=Define

4 CATCHMENT

20.000 ID No.ó 99999
1.590 Area in hectares
102.956 Length (PERV) metres
1.000 Gradient (%)
7.500 Per cent Impervious
102.307 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
74.000 SCS Curve No or C
.100 Ia/S Coefficient
8.924 Initial Abstraction

1 Option 1=Trianglrr; 2=Rectanglrr; 3=SWM HYD; 4=Lin. Reserv
.036 .000 .029 .057 c.m/s

Stormwater Management Plan

Joshua Court Subdivision, Township of West Lincoln

| | | | | | | | |
|----|------------|------------------|--|-------------------|---------------------|----------|--|
| 15 | ADD RUNOFF | .252 | .877 | .299 | C perv/imperv/total | 1 | Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat |
| | | .036 | .036 | .029 | .057 c.m/s | .250 | Manning "n" |
| 11 | CHANNEL | | | | | 74.000 | SCS Curve No or C |
| | | 1.00 | Base Width = | | | .100 | Ia/S Coefficient |
| | | 3.000 | Left bank slope 1: | | | 8.924 | Initial Abstraction |
| | | 3.000 | Right bank slope 1: | | | 1 | Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv |
| | | .040 | Manning's "n" | | | .037 | .340 |
| | | .750 | O/a Depth in metres | | | .252 | .876 |
| | | 1.000 | Select Grade in % | | | .318 | C perv/imperv/total |
| | | Depth = | .147 metres | | | | |
| | | Velocity = | .454 m/sec | | | | |
| | | Flow Capacity = | 2.246 c.m/s | | | | |
| | | Critical depth = | .109 metres | | | | |
| 9 | ROUTE | | | | | 15 | ADD RUNOFF |
| | | 211.000 | Conduit Length | | | 4 | CATCHMENT |
| | | .486 | Supply X-factor <.5 | | | 60.000 | ID No.6 99999 |
| | | 348.695 | Supply K-lag (sec) | | | .360 | Area in hectares |
| | | .500 | Beta weighting factor | | | 48.990 | Length (PERV) metres |
| | | 300.000 | Routing timestep | | | 1.000 | Gradient (%) |
| | | 1 | No. of sub-reaches | | | 5.400 | Per cent Impervious |
| | | .036 | .036 | .036 | .057 c.m/s | 46.990 | Length (IMPERV) |
| 17 | COMBINE | | | | | .000 | %Imp. with Zero Dpth |
| | | 1 | Junction Node No. | | | 1 | Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat |
| | | .036 | .036 | .036 | .087 c.m/s | .250 | Manning "n" |
| 18 | CONFLUENCE | | | | | 74.000 | SCS Curve No or C |
| | | 1 | Junction Node No. | | | .100 | Ia/S Coefficient |
| | | .036 | .087 | .036 | .000 c.m/s | 8.924 | Initial Abstraction |
| 4 | CATCHMENT | | | | | 1 | Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv |
| | | 70.000 | ID No.6 99999 | | | .011 | .377 |
| | | .390 | Area in hectares | | | .252 | .883 |
| | | 50.990 | Length (PERV) metres | | | .286 | C perv/imperv/total |
| | | .500 | Gradient (%) | | | .011 | .386 |
| | | 6.200 | Per cent Impervious | | | | |
| | | 50.990 | Length (IMPERV) | | | | |
| | | .000 | %Imp. with Zero Dpth | | | | |
| | | 1 | Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat | | | | |
| | | .250 | Manning "n" | | | | |
| | | 74.000 | SCS Curve No or C | | | | |
| | | .100 | Ia/S Coefficient | | | | |
| | | 8.924 | Initial Abstraction | | | | |
| | | 1 | Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv | | | | |
| | | .010 | .087 | .036 | .000 c.m/s | | |
| | | .252 | .878 | .291 | C perv/imperv/total | | |
| 15 | ADD RUNOFF | .010 | .095 | .036 | .000 c.m/s | 9 | ROUTE |
| 10 | POND | | | | | | Conduit Length |
| | | 5 | Depth - Discharge - Volume sets | | | | Supply X-factor <.5 |
| | | 192.520 | .000 | .0 | | | Supply K-lag (sec) |
| | | 192.800 | .0140 | 82.1 | | | Beta weighting factor |
| | | 193.060 | .0370 | 209.6 | | | Routing timestep |
| | | 193.400 | .0970 | 424.6 | | | 1 |
| | | 193.700 | .229 | 688.7 | | | No. of sub-reaches |
| | | | | .039 c.m/s | | | |
| | | | | Maximum Depth = | 193.069 metres | | |
| | | | | Maximum Storage = | 215. c.m | | |
| | | .010 | .095 | .039 | .000 c.m/s | | |
| 17 | COMBINE | | | | | 17 | COMBINE |
| | | 2 | Junction Node No. | | | 2 | Junction Node No. |
| | | .010 | .095 | .039 | .039 c.m/s | .011 | .386 |
| 14 | START | | | | | | .386 |
| | | 1 | 1=Zero; 2=Define | | | | .400 c.m/s |
| 35 | COMMENT | | | | | 35 | COMMENT |
| | | 3 | line(s) of comment | | | 3 | line(s) of comment |
| | | * | | | | * | |
| | | OUTLET D | | | | * | |
| | | * | | | | | |
| 4 | CATCHMENT | | | | | 18 | CONFLUENCE |
| | | 80.000 | ID No.6 99999 | | | 2 | Junction Node No. |
| | | 19.770 | Area in hectares | | | .011 | .400 |
| | | 363.043 | Length (PERV) metres | | | | .386 |
| | | .500 | Gradient (%) | | | | .000 c.m/s |
| | | 7.900 | Per cent Impervious | | | | |
| | | 363.043 | Length (IMPERV) | | | | |
| | | .000 | %Imp. with Zero Dpth | | | | |
| | | 1 | Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat | | | | |
| | | .250 | Manning "n" | | | | |
| | | 74.000 | SCS Curve No or C | | | | |
| | | .100 | Ia/S Coefficient | | | | |
| | | 8.924 | Initial Abstraction | | | | |
| | | 1 | Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv | | | | |
| | | .340 | .000 | .039 | .039 c.m/s | | |
| | | .253 | .889 | .303 | C perv/imperv/total | | |
| 15 | ADD RUNOFF | .340 | .340 | .039 | .039 c.m/s | 14 | START |
| 11 | CHANNEL | | | | | 35 | COMMENT |
| | | 1.200 | Base Width = | | | 3 | line(s) of comment |
| | | 3.000 | Left bank slope 1: | | | * | |
| | | 3.000 | Right bank slope 1: | | | OUTLET B | |
| | | .025 | Manning's "n" | | | * | |
| | | .500 | O/a Depth in metres | | | | |
| | | .300 | Select Grade in % | | | | |
| | | Depth = | .252 metres | | | | |
| | | Velocity = | .689 m/sec | | | | |
| | | Flow Capacity = | 1.353 c.m/s | | | | |
| | | Critical depth = | .173 metres | | | | |
| 9 | ROUTE | | | | | 4 | CATCHMENT |
| | | 77.000 | Conduit Length | | | | ID No.6 99999 |
| | | .217 | Supply X-factor <.5 | | | | Area in hectares |
| | | 83.774 | Supply K-lag (sec) | | | | Length (PERV) metres |
| | | .500 | Beta weighting factor | | | | Gradient (%) |
| | | 120.000 | Routing timestep | | | | Per cent Impervious |
| | | 1 | No. of sub-reaches | | | | Length (IMPERV) |
| | | .340 | .340 | .312 | .039 c.m/s | | %Imp. with Zero Dpth |
| 35 | COMMENT | | | | | 17 | COMBINE |
| | | 3 | line(s) of comment | | | 1 | Junction Node No. |
| | | * | | | | .086 | .086 |
| | | OUTLET C | | | | | .083 |
| | | * | | | | | .083 c.m/s |
| 4 | CATCHMENT | | | | | 14 | START |
| | | 50.000 | ID No.6 99999 | | | 1 | 1=Zero; 2=Define |
| | | 1.390 | Area in hectares | | | 4 | CATCHMENT |
| | | 92.263 | Length (PERV) metres | | | | ID No.6 99999 |
| | | 1.000 | Gradient (%) | | | | |
| | | 10.600 | Per cent Impervious | | | | |
| | | 92.263 | Length (IMPERV) | | | | |
| | | .000 | %Imp. with Zero Dpth | | | | |

Stormwater Management Plan

Joshua Court Subdivision, Township of West Lincoln

| | | | |
|-------------------|--|------------------|--|
| .370 | Area in hectares | 35 | COMMENT |
| 49.665 | Length (PERV) metres | 3 | line(s) of comment |
| .500 | Gradient (%) | * | |
| 39.500 | Per cent Impervious | OUTLET D | |
| 49.665 | Length (IMPERV) | * | |
| .000 | %Imp. with Zero Dpth | 4 | CATCHMENT |
| 1 | Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat | 80.000 | ID No.6 99999 |
| .250 | Manning "n" | 19.770 | Area in hectares |
| 74.000 | SCS Curve No or C | 363.043 | Length (PERV) metres |
| .100 | Ia/S Coefficient | .500 | Gradient (%) |
| 8.924 | Initial Abstraction | 7.900 | Per cent Impervious |
| 1 | Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv | 363.043 | Length (IMPERV) |
| .091 | .000 | .083 | .083 c.m/s |
| .456 | .932 | .644 | C perv/imperv/total |
| 15 | ADD RUNOFF | .250 | %Imp. with Zero Dpth |
| .091 | .091 | .083 | Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat |
| 11 | CHANNEL | .250 | Manning "n" |
| .100 | Base Width = | 74.000 | SCS Curve No or C |
| 3.000 | Left bank slope 1: | .100 | Ia/S Coefficient |
| 3.000 | Right bank slope 1: | 8.924 | Initial Abstraction |
| .040 | Manning's "n" | 1 | Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv |
| .600 | O/a Depth in metres | 1.270 | .000 |
| .500 | Select Grade in % | .456 | .211 |
| Depth = | .246 metres | .944 | .495 |
| Velocity = | .441 m/sec | | C perv/imperv/total |
| Flow Capacity = | .888 c.m/s | 15 | ADD RUNOFF |
| Critical depth = | .164 metres | 1.270 | 1.270 |
| 9 | ROUTE | .211 | .211 c.m/s |
| 76.000 | Conduit Length | 11 | CHANNEL |
| .371 | Supply X-factor <.5 | 1.200 | Base Width = |
| 129.326 | Supply K-lag (sec) | 3.000 | Left bank slope 1: |
| .500 | Beta weighting factor | 3.000 | Right bank slope 1: |
| 150.000 | Routing timestep | .025 | Manning's "n" |
| 1 | No. of sub-reaches | .515 | O/a Depth in metres |
| .091 | .091 | .300 | Select Grade in % |
| .083 | .083 c.m/s | Depth = | .485 metres |
| 17 | COMBINE | Velocity = | .986 m/sec |
| 1 | Junction Node No. | Flow Capacity = | 1.440 c.m/s |
| .091 | .091 | Critical depth = | .360 metres |
| .083 | .166 c.m/s | 9 | ROUTE |
| 14 | START | 77.000 | Conduit Length |
| 1 | 1=Zero; 2=Define | .000 | Supply X-factor <.5 |
| 4 | CATCHMENT | 58.581 | Supply K-lag (sec) |
| 20.000 | ID No.6 99999 | .500 | Beta weighting factor |
| 1.590 | Area in hectares | 100.000 | Routing timestep |
| 102.956 | Length (PERV) metres | 1 | No. of sub-reaches |
| 1.000 | Gradient (%) | 1.270 | 1.270 |
| 7.500 | Per cent Impervious | 1.263 | .211 c.m/s |
| 102.307 | Length (IMPERV) | 35 | COMMENT |
| .000 | %Imp. with Zero Dpth | 3 | line(s) of comment |
| 1 | Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat | * | |
| .250 | Manning "n" | OUTLET C | |
| 74.000 | SCS Curve No or C | * | |
| .100 | Ia/S Coefficient | 4 | CATCHMENT |
| 8.924 | Initial Abstraction | 50.000 | ID No.6 99999 |
| 1 | Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv | 1.390 | Area in hectares |
| .221 | .000 | 92.263 | Length (PERV) metres |
| .456 | .934 | 1.000 | Gradient (%) |
| .492 | .166 c.m/s | 10.600 | Per cent Impervious |
| 15 | ADD RUNOFF | 92.263 | Length (IMPERV) |
| .221 | .221 | .083 | .083 c.m/s |
| .166 | .166 c.m/s | .000 | %Imp. with Zero Dpth |
| 11 | CHANNEL | 1 | Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat |
| .100 | Base Width = | .250 | Manning "n" |
| 3.000 | Left bank slope 1: | 74.000 | SCS Curve No or C |
| 3.000 | Right bank slope 1: | .100 | Ia/S Coefficient |
| .040 | Manning's "n" | 8.924 | Initial Abstraction |
| .750 | O/a Depth in metres | 1 | Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv |
| 1.000 | Select Grade in % | .200 | 1.270 |
| Depth = | .305 metres | .454 | .935 |
| Velocity = | .714 m/sec | .505 | C perv/imperv/total |
| Flow Capacity = | 2.246 c.m/s | 15 | ADD RUNOFF |
| Critical depth = | .240 metres | .200 | 1.342 |
| 9 | ROUTE | 1.263 | .211 c.m/s |
| 211.000 | Conduit Length | 4 | CATCHMENT |
| .471 | Supply X-factor <.5 | 60.000 | ID No.6 99999 |
| 221.722 | Supply K-lag (sec) | .360 | Area in hectares |
| .500 | Beta weighting factor | 48.990 | Length (PERV) metres |
| 200.000 | Routing timestep | 1.000 | Gradient (%) |
| 1 | No. of sub-reaches | 5.400 | Per cent Impervious |
| .221 | .221 | 46.990 | Length (IMPERV) |
| .205 | .166 c.m/s | .000 | %Imp. with Zero Dpth |
| 17 | COMBINE | 1 | Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat |
| 1 | Junction Node No. | .250 | Manning "n" |
| .221 | .221 | 74.000 | SCS Curve No or C |
| .205 | .332 c.m/s | .100 | Ia/S Coefficient |
| 18 | CONFLUENCE | 8.924 | Initial Abstraction |
| 1 | Junction Node No. | 1 | Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv |
| .221 | .332 | .062 | 1.342 |
| .205 | .000 c.m/s | .455 | .923 |
| 4 | CATCHMENT | .480 | C perv/imperv/total |
| 70.000 | ID No.6 99999 | 15 | ADD RUNOFF |
| .390 | Area in hectares | .062 | 1.358 |
| 50.990 | Length (PERV) metres | 1.263 | .211 c.m/s |
| .500 | Gradient (%) | 9 | ROUTE |
| 6.200 | Per cent Impervious | .000 | Conduit Length |
| 50.990 | Length (IMPERV) | .500 | Supply X-factor <.5 |
| .000 | %Imp. with Zero Dpth | .000 | Supply K-lag (sec) |
| 1 | Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat | .500 | Beta weighting factor |
| .250 | Manning "n" | 600.000 | Routing timestep |
| 74.000 | SCS Curve No or C | 1 | No. of sub-reaches |
| .100 | Ia/S Coefficient | .062 | 1.358 |
| 8.924 | Initial Abstraction | 1.358 | .211 c.m/s |
| 1 | Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv | 17 | COMBINE |
| .059 | .332 | 2 | Junction Node No. |
| .456 | .933 | .062 | 1.358 |
| .486 | .000 c.m/s | 1.358 | 1.569 c.m/s |
| 15 | ADD RUNOFF | 35 | COMMENT |
| .059 | .391 | 3 | line(s) of comment |
| .205 | .000 c.m/s | * | |
| 10 | POND | OUTLET E | |
| 5 | Depth - Discharge - Volume sets | * | |
| 192.520 | .000 | CONFLUENCE | |
| 192.800 | .0140 | 2 | Junction Node No. |
| 193.060 | .0370 | .062 | 1.569 |
| 193.400 | .0970 | 1.358 | .000 c.m/s |
| 193.700 | .229 | 20 | MANUAL |
| Peak Outflow = | .211 c.m/s | | |
| Maximum Depth = | 193.660 metres | | |
| Maximum Storage = | 654. c.m | | |
| .059 | .391 | .211 | .000 c.m/s |
| 17 | COMBINE | | |
| 2 | Junction Node No. | | |
| .059 | .391 | .211 | .211 c.m/s |
| 14 | START | | |
| 1 | 1=Zero; 2=Define | | |